



## **Introduction to Electrical Networks**

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### **Chapter Four**

#### **The Filters**

##### **Part 3**

- ***Butterworth Filter***
- ***Analog to analog transformations***
- ***Design of Low Pass Butterworth Filters***

## 4.8 Butterworth Filter

The Butterworth filter is a type of signal-processing filter designed to have a frequency response that is as flat as possible in the passband as shown in Fig. (4.12). It is also referred to as a maximally flat magnitude filter. It was first described in 1930 by the British engineer and physicist **Stephen Butterworth**. A Butterworth filter is a filter with an amplitude response of:-

$$|H_n(j\omega)| = \frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_c}\right)^{2n}}} \quad \dots (20)$$

Where  $\omega_c$  is the cutoff frequency and  $n$  is the filter order.

We will design a normalized filter (taking  $\omega_c = 1 \text{ rad/sec}$ ), and then scale filter to the desired cutoff frequency, so evaluating ( $\omega_c = 1 \text{ rad/sec}$ ) this will lead Eq. (20) to be:-

$$|H_n(j\omega)| = \frac{1}{\sqrt{1 + \omega^{2n}}} \quad \dots (21)$$

Note that

$$|H_n(j\omega)|^2 = H_n(j\omega)H_n(-j\omega) = \frac{1}{1 + \omega^{2n}} \quad \dots (22)$$

So, to find the transfer function of the mentioned filter we applied the below points:-

- 1- The transfer function of the filter is denoted as  $H_n(s)$ .
- 2- Recall that  $s = \sigma + j\omega$ .
- 3- The frequency response  $H_n(j\omega)$  can be obtained from  $H_n(s)$  by evaluating  $s = j\omega$ , ie  $\omega = s/j$ .
- 4- Applying the aforementioned points in Eq. (22), we will get

$$|H_n(j\omega)|^2 = H_n(j\omega)H_n(-j\omega) = H_n(s)H_n(-s) = \frac{1}{1 + (s/j)^{2n}} \quad \dots (23)$$

Since  $H_n(s)H_n(-s) = \frac{1}{1 + (s/j)^{2n}}$ ,  $H_n(s)H_n(-s)$  has  $2n$  poles, and they occur when:-

$$(s/j)^{2n} = -1 \quad \dots (24)$$

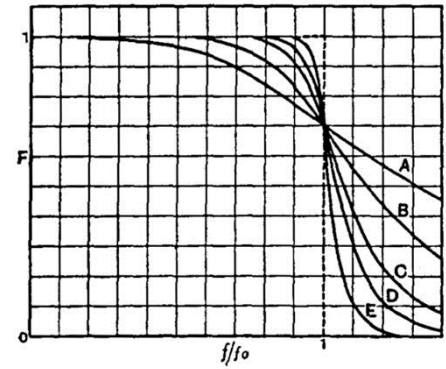


Fig. 3.

Fig 4.12 The frequency response plot from Butterworth's 1930 paper.

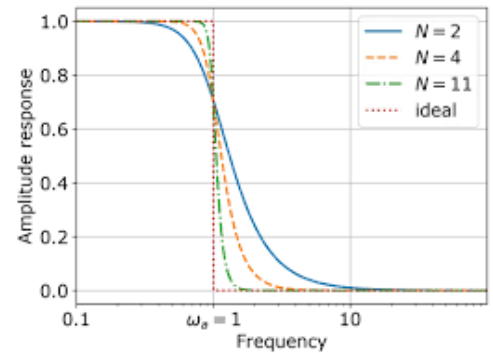


Fig 4.13 The frequency response plot of several Butterworth filter.

Isolating  $s$  yields

$$s^{2n} = -(j)^{2n} \quad \dots (25)$$

Since  $-1 = e^{j\pi(2k-1)}$  for integer  $k$ , and  $-j = e^{j\pi/2}$ , Eq. (25) will be

$$s^{2n} = e^{j\pi(2k-1+n)} \quad \dots (26)$$

Taking  $1/2n$  root of the each side of Eq. (20) yields

$$s = e^{\frac{j\pi}{2n}(2k-1+n)} = \cos\left(\frac{\pi}{2n}(2k-1+n)\right) + j \sin\left(\frac{\pi}{2n}(2k-1+n)\right) \quad \dots (27)$$

For  $k = 1, 2, \dots, 2n$ .

From Eq. (27), it is clear that the poles will be located in a unit circle with the origin center as shown in Fig. 4.14.

From Fig. 4.14, the left  $n$  poles are corresponded to  $H_n(s)$ , while the right  $n$  poles are corresponded to  $H_n(-s)$ .

If we wish the filter  $H_n(s)$  to be stable, the poles of  $H_n(s)$  are selected to be those in the left half plane and  $H_n(s)$  can be written in the following form:

$$\begin{aligned} H_n(s) &= \frac{1}{(s - s_1)(s - s_2) \dots (s - s_n)} \\ &= \frac{1}{s^n + a_{n-1}s^{n-1} + a_{n-2}s^{n-2} + \dots + 1} \\ &= \frac{1}{B_n(s)} \quad \dots (28) \end{aligned}$$

Where  $B_n(s)$  is  $n$ th order Butterworth Polynomial.

According to the above  $H_n(s)$  can be computed by Hand or by evaluating the value of  $B_n(s)$  in Table 4.1.

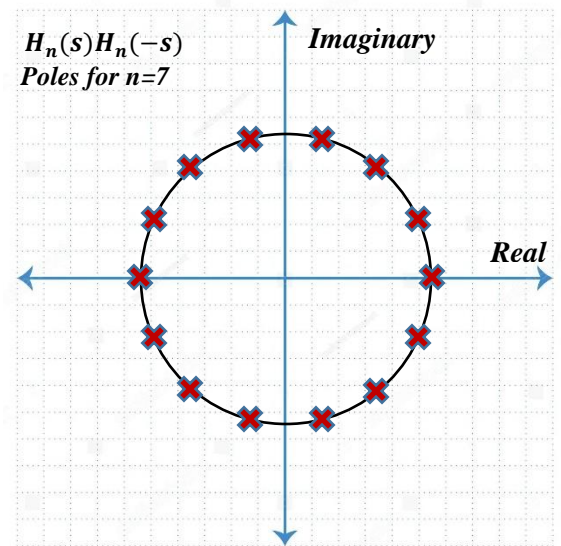


Fig 4.14 Poles distribution of seventh order Butterworth Filter.

**Table 4.1 Factors of Butterworth polynomials of order 1 through 10.**

n	Factors of Butterworth Polynomials $B_n(s)$
1	$(s + 1)$
2	$(s^2 + 1.414214s + 1)$
3	$(s + 1)(s^2 + s + 1)$
4	$(s^2 + 0.765367s + 1)(s^2 + 1.847759s + 1)$
5	$(s + 1)(s^2 + 0.618034s + 1)(s^2 + 1.618034s + 1)$
6	$(s^2 + 0.517638s + 1)(s^2 + 1.414214s + 1)(s^2 + 1.931852s + 1)$
7	$(s + 1)(s^2 + 0.445042s + 1)(s^2 + 1.246980s + 1)(s^2 + 1.801938s + 1)$
8	$(s^2 + 0.390181s + 1)(s^2 + 1.111140s + 1)(s^2 + 1.662939s + 1)(s^2 + 1.961571s + 1)$
9	$(s + 1)(s^2 + 0.347296s + 1)(s^2 + s + 1)(s^2 + 1.532089s + 1)(s^2 + 1.879385s + 1)$
10	$(s^2 + 0.312869s + 1)(s^2 + 0.907981s + 1)(s^2 + 1.414214s + 1)(s^2 + 1.782013s + 1)(s^2 + 1.975377s + 1)$

### **4.8.1 Analog to analog transformations:**

In the following discussion, a normalized low-pass filter will be used as a prototype filter for illustration. For normalization purposes we selected  $\omega_c = 1 \text{ rad/sec}$ . For the other values of  $\omega_c$ , a scaling will be performed to  $H_n(s)$  in Table 4.1 by replacing  $s$  with  $s/\omega_c$ .

$$H'(s) = H(s)|_{s \rightarrow s/\omega_c} = H(s/\omega_c) \quad \dots (29)$$

For the other types of filters, we apply Table 4.2 scaling.

**Table 4.2 Normalizing Butterworth Filters .**

<i>Filter Type</i>	<i>Prototype response</i>	<i>Transformed filter response</i>
<i>Low-pass filter</i>	Normalized Low-pass $G(s)$	$H(s) = G(s) _{s \rightarrow s/\omega_c}$
<i>High-pass filter</i>	Normalized Low-pass $G(s)$	$H(s) = G(s) _{s \rightarrow \omega_c/s}$
<i>Band-pass filter</i>	Normalized Low-pass $G(s)$	$H(s) = G(s) _{s \rightarrow \frac{s^2 + \omega_l \omega_u}{s(\omega_u - \omega_l)}}$
<i>Band-stop filter</i>	Normalized Low-pass $G(s)$	$H(s) = G(s) _{s \rightarrow \frac{s(\omega_u - \omega_l)}{s^2 + \omega_l \omega_u}}$

## 4.8.2 Design of Low Pass Butterworth Filters

The filter requirements are normally given in terms of a set of critical frequency, say  $\omega_p$ ,  $\omega_s$  and gains  $G_p$ ,  $G_s$ . A common set of conditions for the low-pass response is given in Fig. 4.15.

The dB Gain for any  $\omega_x$  is

$$G_x = 20 \log_{10} |H_n(j\omega_x)| = 20 \log_{10} \left( \frac{1}{\sqrt{1 + \left(\frac{\omega_x}{\omega_c}\right)^{2n}}} \right) = 0 - 20 = -10 \log_{10} \left( 1 + \left(\frac{\omega_x}{\omega_c}\right)^{2n} \right) \quad \dots (30)$$

So, gains at frequencies  $\omega_p$ ,  $\omega_s$  are

$$G_{p,dB} = -10 \log_{10} \left( 1 + \left(\frac{\omega_p}{\omega_c}\right)^{2n} \right) \quad \Rightarrow \quad \left(\frac{\omega_p}{\omega_c}\right)^{2n} = 10^{-\frac{G_{p,dB}}{10}} - 1 \quad \dots (31)$$

$$G_{s,dB} = -10 \log_{10} \left( 1 + \left(\frac{\omega_s}{\omega_c}\right)^{2n} \right) \quad \Rightarrow \quad \left(\frac{\omega_s}{\omega_c}\right)^{2n} = 10^{-\frac{G_{s,dB}}{10}} - 1 \quad \dots (32)$$

Dividing Eq. (32) to Eq. (31), yields

$$\left(\frac{\omega_s}{\omega_p}\right)^{2n} = \frac{10^{-\frac{G_{s,dB}}{10}} - 1}{10^{-\frac{G_{p,dB}}{10}} - 1} \quad \dots (33)$$

By solving Eq. (30), gets

$$n = \frac{\log_{10} \left[ \frac{10^{-\frac{G_{s,dB}}{10}} - 1}{10^{-\frac{G_{p,dB}}{10}} - 1} \right]}{2 \log_{10}(\omega_s/\omega_p)} \quad \dots (34)$$

Solving Eq. (31 & 32), yields

$$\omega_c = \omega_p / \left( 10^{-\frac{G_{p,dB}}{10}} - 1 \right)^{\frac{1}{2n}} \quad \dots (35)$$

$$\omega_c = \omega_s / \left( 10^{-\frac{G_{s,dB}}{10}} - 1 \right)^{\frac{1}{2n}} \quad \dots (36)$$

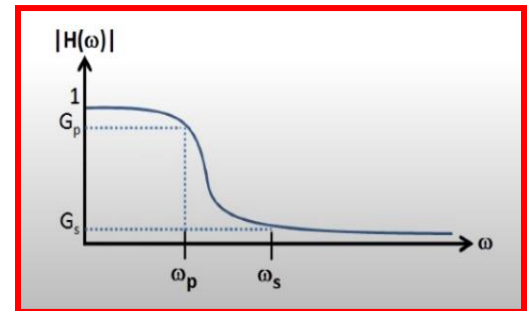


Fig 4.15 Butterworth low pass filter specifications.

**Example 4.4:-** Design a low-pass Butterworth filter with below specifications:-

$$G_{p,dB} = -3 \text{ dB}, G_{s,dB} = -25 \text{ dB}, \omega_p = 20 \text{ rad/sec} \quad \& \quad \omega_s = 50 \text{ rad/sec}$$

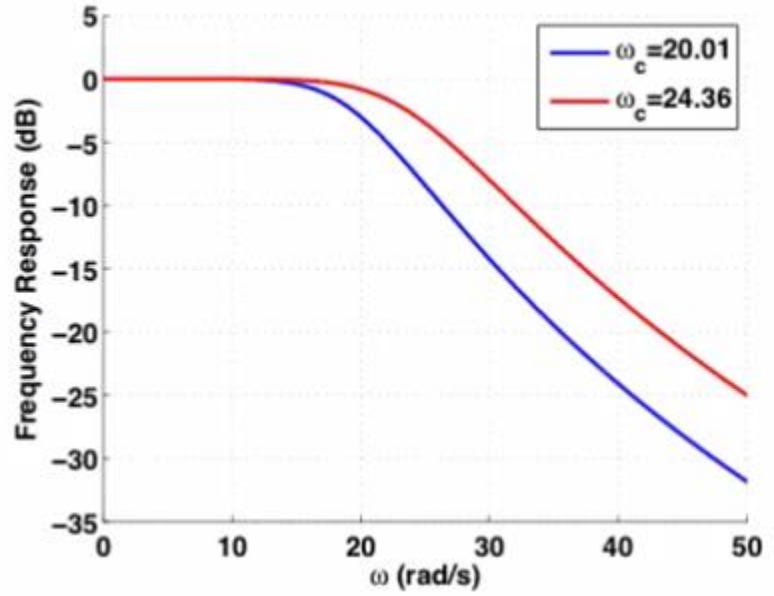


Fig 4.15 For Example 4.4.