

# Design of Single Reinforced Rectangular Beam Sections

(Design of SRRS)

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Before getting into design it is good to introduce the following new three terms or definitions:

$$\rho = \frac{A_s}{bd}$$

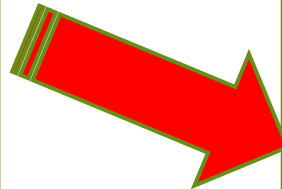
$$m = \frac{f_y}{0.85 f'_c}$$

$$R_n = \frac{M_n}{bd^2}$$

$$A_s f_y = 0.85 f'_c a b \quad (1)$$

$$M_n = A_s f_y \left( d - \frac{a}{2} \right) \quad (2)$$

$$\varepsilon_t = 0.003 \left( \frac{d_t - c}{c} \right) \quad (3)$$



$$a = \rho m d \quad (1')$$

$$R_n = \frac{M_n}{bd^2} = \rho f_y \left( 1 - \frac{1}{2} \rho m \right) \quad (2')$$

$$\rho = \left( \frac{0.003}{0.003 + \varepsilon_s} \right) \frac{\beta_1}{m} \left( \frac{d_t}{d} \right) \quad (3')$$

$$\rho = \frac{1}{m} \left( 1 - \sqrt{1 - \frac{2m R_n}{f_y}} \right) \quad (4')$$

As an example of usefulness of the above (dash equations) we can calculate  $\rho_b$  and  $\rho_{max}$  for ( $f_y=420\text{MPa}$ ) by substituting  $\epsilon_s=0.002$  and  $\epsilon_s=0.005$  in eq.(3') respectively:

$$\rho_b = \frac{3 \beta_1}{5 m} \left( \frac{d_t}{d} \right) \quad \text{for } f_y = 420 \text{ MPa because } \epsilon_y = 0.002$$

$$\rho_{max} = \frac{3 \beta_1}{8 m} \left( \frac{d_t}{d} \right) \quad \text{for all Cases}$$

Or in design problems we can start estimating the  $A_s$  by assuming  $\epsilon_s=0.007$  to stay in Tension Control Zone so:

$$\rho_{start} = \frac{3 \beta_1}{10 m} \left( \frac{d_t}{d} \right)$$

Design problems will mainly depend on eq.(2')

$$R_n = \frac{M_n}{bd^2} = \rho f_y \left( 1 - \frac{1}{2} \rho m \right) \quad (2')$$

**Table 9.3.1.1—Minimum depth of nonprestressed beams**

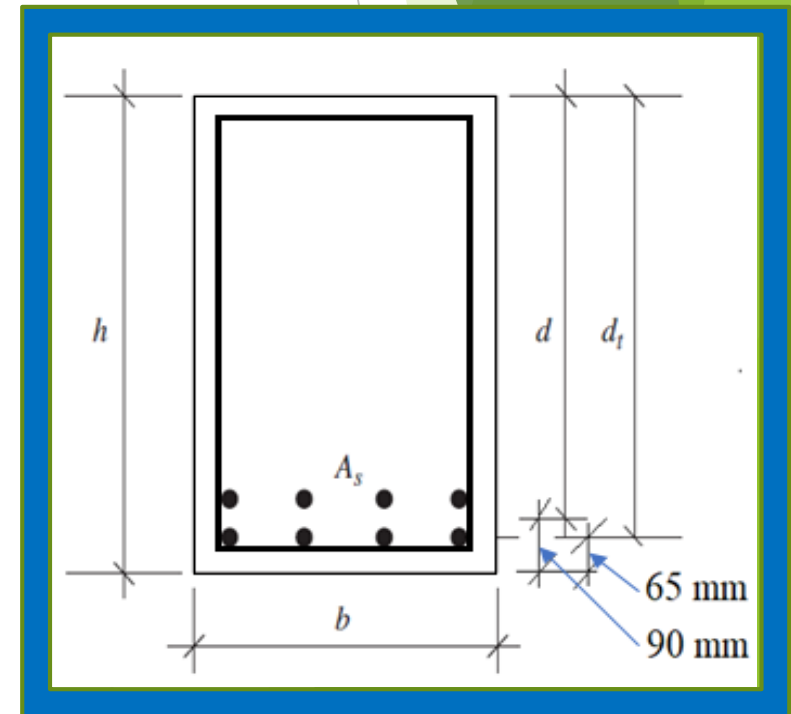
Support condition	Minimum $h^{[1]}$
Simply supported	$\ell/16$
One end continuous	$\ell/18.5$
Both ends continuous	$\ell/21$
Cantilever	$\ell/8$

$$h = [1.5 \text{ to } 2] \times b$$

Minimum concrete cover for beams=40mm

ACI 25.2.1 the minimum clear bar spacing:

$$S_{min} \geq \begin{cases} 25mm \\ d_b \\ \left(\frac{4}{3}\right) d_{agg} \end{cases}$$



**Ex1: Find the necessary reinforcement for a given section that has a width of 250mm and total depth of 500mm, if it is subjected to a factored moment of 180kN.m. Given  $f'_c=21\text{Mpa}$ ,  $f_y=375\text{MPa}$ .**

**Solution:**

$$\varepsilon_y = \frac{f_y}{E_s} = \frac{375}{200000} = 0.001875$$

$$m = \frac{f_y}{0.85 f'_c} = \frac{375}{0.85 \times 21} = 21.0$$

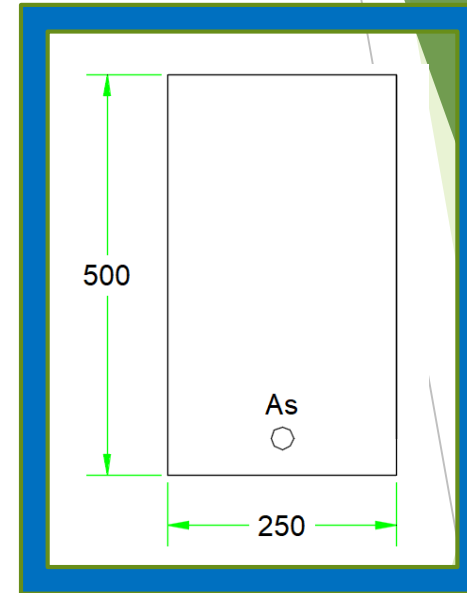
$$M_n = \frac{180}{0.9} = 200 \text{ kN.m}$$

Assume one layer of reinforcement

$$d = h - 65 = 500 - 65 = 435\text{mm}$$

$$R_n = \frac{M_n}{bd^2}$$

$$R_n = \frac{200 \times 10^6}{250 \times 435^2} = 4.227$$



$$\rho = \frac{1}{m} \left( 1 - \sqrt{1 - \frac{2m R_n}{f_y}} \right)$$

$$\rho = \frac{1}{21} \left( 1 - \sqrt{1 - \frac{2 \times 21 \times 4.227}{375}} \right) = 0.013$$

$$\rho_{max} = \frac{3 \beta_1}{8 m} \left( \frac{d_t}{d} \right)$$

$$\rho_{max} = \frac{3 \times 0.85}{8 \times 21.0} (1) = 0.0151 > 0.013 \text{ (ok Tension control)}$$

$$A_s = \rho b d = 0.013 \times 250 \times 435 = 1413.75 \text{ mm}^2$$

Try  $\emptyset 25 \rightarrow A_b = 490 \text{ mm}^2$

$$n = \frac{A_s}{A_b} = \frac{1413.75}{490} = 2.88$$

Use 3 Ø25

$$A_{S_{provided}} = 3 \times 490 = 1470 \text{ mm}^2$$

$$\rho_{provided} = \frac{1470}{250 \times 435} = 0.0135 < 0.0151 \text{ (ok T.C)}$$

$$\rho_{min} = \frac{1.4}{f_y} = \frac{1.4}{375} = 0.00373 < 0.0135 \text{ (ok)}$$

Check for bar spacing:

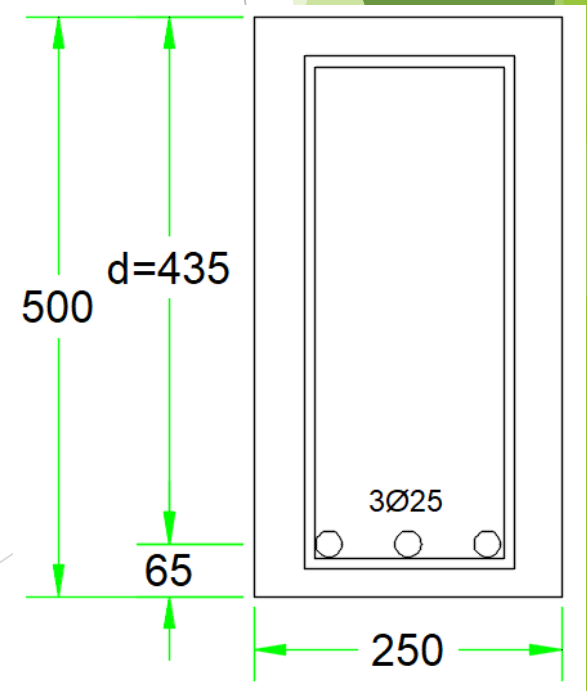
$$S_{min} = \begin{cases} 25\text{mm} \\ d_b = 25 \\ \left(\frac{4}{3}\right) d_{agg} = \frac{4}{3} \times 20 = 26.66 \end{cases}$$

$$s = \frac{250 - 100 - 3 \times 25}{2} = 37.5 > 26.66 \text{ (ok)}$$

$$M_n = \rho f_y b d^2 \left(1 - \frac{1}{2} \rho m\right)$$

$$M_n = 0.0135 \times 375 \times 250 \times 435^2 \left(1 - \frac{1}{2} \times 0.0135 \times 21.0\right) = 205.54 \text{ kN.m}$$

$$M_u = \phi M_n = 0.9 \times 205.54 = 184.98 \text{ kN.m} > 180 \text{ (OK)}$$



**Ex2: Design a rectangular section to resist a factored moment of 300kN.m. Given  $f'_c=28\text{MPa}$ , and  $f_y=420\text{MPa}$ .**

**Solution:**

$$M_n = \frac{M_u}{\phi} = \frac{300}{0.9} = 333.33 \text{ kN.m}$$

$$m = \frac{f_y}{0.85 f'_c} = \frac{420}{0.85 \times 28} = 17.647$$

$$R_n = \frac{M_n}{bd^2} = \rho f_y \left( 1 - \frac{1}{2} \rho m \right)$$

Start with  $\rho$  depending on  $\epsilon_s=0.007$  and assuming one layer of reinforcement:

$$\rho_{start} = \frac{3 \beta_1}{10 m} \left( \frac{d_t}{d} \right)$$

$$\rho_{start} = \left( \frac{3}{10} \right) \frac{0.85}{17.647} (1) = 0.0144$$

$$R_n = \rho f_y \left( 1 - \frac{1}{2} \rho m \right)$$



$$R_n = 0.0144 \times 420 \left( 1 - \frac{1}{2} \times 0.0144 \times 17.647 \right) = 5.277$$

$$R_n = \frac{M_n}{bd^2}$$

$$5.277 = \frac{333.33 \times 10^6}{bd^2}$$

$$bd^2 = 63166571.92 \text{ mm}^3$$

Assume b to get d:

b	d	d/b
250	502.66	2.01
300	458.86	1.529
350	424.82	1.213

$$A_s = \rho b d = 0.0144 \times 300 \times 460 = 1987.2 \text{ mm}^2$$

Try  $\emptyset 22 \rightarrow A_b = 380$

$$n = \frac{1987.2}{380} = 5.23$$

Use 6Ø22 in two layers:

$$A_{s_{provided}} = 6 \times 380 = 2280 \text{ mm}^2$$

$$\rho_{provided} = \frac{2280}{300 \times 460} = 0.0165$$

$$\rho_{max} = \frac{3 \beta_1}{8 m} \left( \frac{d_t}{d} \right)$$

$$\rho_{max} = \frac{3}{8} \times \frac{0.85}{17.647} \times \left( \frac{489}{460} \right) = 0.0192 > 0.0165 \text{ (ok T.C)}$$

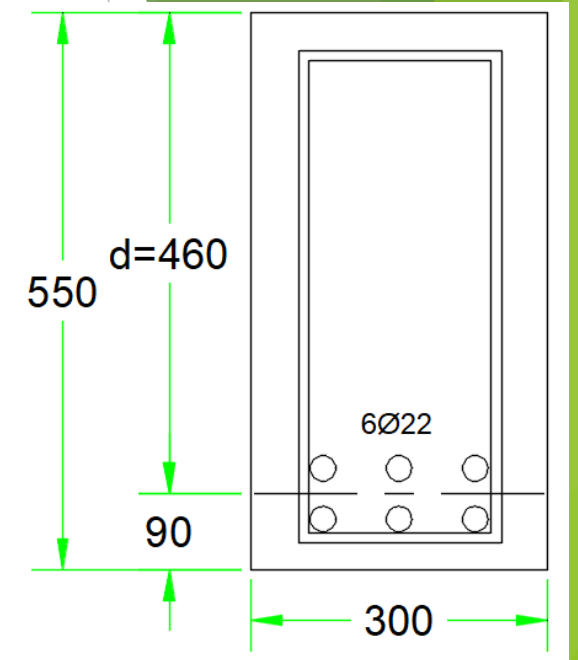
$$\rho_{min} = \frac{1.4}{f_y} = \frac{1.4}{420} = 0.00333 < 0.0165 \text{ (ok)}$$

$$h = d + 90 = 460 + 90 = 550 \text{ mm}$$

$$s = \frac{300 - 100 - 3 \times 22}{2} = 67 > 26.66 \text{ (ok)}$$

$$M_n = 0.0165 \times 420 \times 300 \times 460^2 \left( 1 - \frac{1}{2} \times 0.0165 \times 17.647 \right) = 375.87 \text{ kN.m}$$

$$M_u = \phi M_n = 0.9 \times 375.87 = 338.283 \text{ kN.m} > 300 \text{ (OK)}$$



**Thank you...**