

NONLINEAR OPTICAL PROPERTIES AND OPTICAL POWER LIMITING OF POLY (3HT- Co - Th) - PMMA POLYMER BLEND FILMS



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1. INTRODUCTION

ABSTRACT

Poly (3 - Hexylthiophene - Co - Thiophene) copolymer was prepared using the addition polymerization method and poly (3HT- Co - Th) – PMMA polymer blend films were prepared using the casting method. The nonlinear optical properties and the behavior of the optical power limiting of the prepared films were studied using the z - scan technique for different weight ratios of the copolymer poly (3HT- Co - Th). In the present work, a continuous wave (CW) diode - pumped solid - state laser (DPSSL) of wavelengths 532 nm was used for the irradiation of the prepared film samples. The nonlinear optical parameters such as, the nonlinear refractive index (n2), the nonlinear absorption coefficient (β), and the third - order nonlinear optical susceptibility (χ ⁽³⁾) of the polymer blend poly (3HT- Co -Th) - PMMA films were determined for different weight ratios of the copolymer poly (3HT- Co - Th). It is observed that the polymer blend poly (3HT - Co - Th) - PMMA films exhibit saturable absorption (SA) and self defocusing effects, and this gives an indication that both, the nonlinear refractive index (n2) and the nonlinear absorption coefficient (β) , have negative values. The obtained results indicate that the prepared polymer blend poly (3HT - Co - Th) - PMMA films are promising materials and can be considered as suitable materials for different optical and electronic applications.

Nonlinear optical (NLO) properties of different optical materials have received much attention because of their several applications such as, optical power limiting, optical switching, light - emitting diodes, solar cells, optical sensors, and in photonic and optoelectronic devices [1 - 17]. Thiophone is one of these important materials. It is a conjugate polymer and has attractive properties for many optical and electronic applications, such as: Solubility in the organic solvents, flexibility in the preparation, and absorbance in the ultraviolet and visible spectral regions, high electrical conductivity, good environmental stability, and high optical damage thresholds [8, 18]. Thiophene and 3 - Hexylthiophene were used to prepared the copolymer poly (3HT- Co - Th). In order to obtain a new polymer suitable for the optical and optoelectronic applications, the prepared copolymer is adding to the poly (methyl methacrylate) (PMMA) polymer. Such prepared polymer blend shows high absorption in the range of the visible and the ultraviolet of the electromagnetic spectrum. It is observed that the addition of the prepared copolymer to the PMMA polymer causes significant modification in the optical properties of the PMMA polymer. It is found, in the present study, that

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the optical properties of the prepared polymer blend poly (3HT- Co - Th) - PMMA films are depended on the weight ratio of the added copolymer poly (3HT - Co - Th) to the PMMA polymer and their properties are changed with changing this weight ratio.

Optical limiting (OPL) behavior is an important nonlinear effect can be used for the optical limiter device to protect the human eyes and the other sensitive optical devices (such as, optical switches and optical sensors), from the optical damages due to the intense laser beams, that may be caused those damages. The optical limiter is working as an attenuator for the incident optical radiation (such as the laser beam radiation) on these devices. In the nonlinear optical materials, the output power (or the intensity) of the laser beam tends to increase with increasing the input power (or the intensity) of the laser beam until it reaches a value called the threshold optical power (P_{th}), then the output power starts to stabilize at a constant value as the input power continuing to increase [19 - 24].

There are several techniques for measuring the nonlinear optical properties of the optical materials. The z - scan technique is one of these techniques, which is commonly used for the measurements of the nonlinear optical properties of the optical materials due to its advantages such as, the simplicity of the experimental setup and the optical measurements, as well as it is easily to interpret the results that obtained from the optical measurements. Moreover, this technique is sensitive to most the nonlinear optical effects such as, self - focusing, self - defocusing, nonlinear refraction, nonlinear saturable absorption (SA), and optical limiting [25, 29]. This technique can be used to measure the nonlinear refractive index (n₂), the nonlinear absorption coefficient (β), and the third - order of the nonlinear optical susceptibility (χ ⁽³⁾) of many optical materials. There are two types of the z - scan technique. The first type is called, close - aperture z - scan, is used to scan the beam of the laser along the z - axis of the closed (partially open) aperture and measure the nonlinear refractive index (n₂). While the second type is called, the open - aperture z - scan (the aperture is completely open or it is removed from the z - scan system) and is used to measure the nonlinear absorption coefficient (β). In addition to being used to measure the real and imaginary parts of the third - order nonlinear optical susceptibility (χ ⁽³⁾), this technique is also used to study the properties of the optical power limiting.

2. EXPERIMENTAL METHODS AND MEASUREMENTS

The copolymer poly (3HT - Co - Th) was prepared by using the addition polymerization method. The monomers 3HT and Th were purchased from the Aman International Industrial Company, India. Two different weight ratios of the 3HT and TH monomers were mixed together. The poly (3HT - Co - Th) - PMMA polymer blend film samples were prepared for different weight ratios by using the casting method. 4 gm of poly(methylmethacrylate) (PMMA) polymer was dissolved in 10 ml of Chloroform and the mixture was stirred for 3 hours until the polymer completely dissolved and homogenous solution produced. Then, different percentage weight ratios of the copolymer poly (3HT - Co - Th), 0.033 %, 0.040 %, 0.046 %, 0.053 %, and 0.060% were added to the PMMA solution. The produced solution was stirred until the two polymers mixed together and homogeneous solutions were formed. The produced solutions of the poly (3HT - Co - Th) - PMMA polymer blend at different weight ratios of the copolymer poly (3HT - Co - Th) were cast on glass slides of 1 mm thickness and left to dry progressively and hard poly (3HT - Co - Th) - PMMA polymer blend. The average thickness of these films was around 1 mm.

The absorbance (A) and the transmittance (T) spectra of the prepared polymer film samples were measured by using Cecil UV - Visible double - beam spectrophotometer (Model CE -7500) of the wavelength range 190 - 1100 nm.

For measuring the nonlinear optical properties and determining the associated nonlinear optical parameters of the poly (3HT - Co - Th) - PMMA polymer blend films, the z - scan technique was used. Fig.1. shows the schematic diagram of the z - scan experimental setup used in the present work for the measurements of the nonlinear optical properties of the prepared poly (3HT - Co - Th) - PMMA polymer blend films.

The laser used in the z - scan experiments was a continuous wave (CW) diode - pumped solid - state laser (DPSSL) of a Gaussian beam at λ = 532 nm wavelength. The laser is of adjustable output power over the range 0 - 100 mW. A converging lens (L) of focal length 5 cm was used to focus the laser beam on the film sample. The radius of the laser beam (w₀) at the beam waist is approximately 18 µm, and the intensity of the laser beam is calculated and its value is I₀ = 1.94 kW / cm². The corresponding Rayleigh range (Z_R) is 1.91 mm, which is consisted with the z - scan condition that the length of the sample (L) must be less than the Rayleigh range (Z_R), namely, L << ZR [22]. The output laser beam was spitted into two parts by the beam splitter (BS). The first part of the laser beam is directed toward the photo-detector D₁, which was used to measure the power of the incident laser beam on the sample. While the second

part of the laser beam was focused on the film sample by the convergence lens (L) and passes through the sample. Then the laser beam passes through the narrow aperture and incident on the photo-detector D_2 , which was placed behind the aperture to measure the power of the transmitted beam. The radius of the aperture, which used in the closed (partially open) aperture, is 1 mm.



Figure 1: Schematic diagram of the z - scan experimental setup used for the measurements of the nonlinear optical properties of the prepared film samples.

3. RESULTS AND DISCUSSION

UV - Visible absorbance spectra of the poly (3HT - Co - Th) - PMMA polymer blend films for different weight ratios of the copolymer poly (3HT - Co - Th) were recorded over the wavelengths 300 - 900 nm by using the double - beam spectrophotometer, as shown in Fig. 2. The spectra show that the high absorbance peaks are located around the wavelength 466 nm. The values of absorbance are in the range of 0.05 - 0.34 (Arb. Units) for the weight ratios range 0.033 % - 0.060 % of the copolymer poly (3HT - Co - Th). It can be clearly seen that the value of the absorbance of the poly (3HT - Co - Th) - PMMA polymer blend film increases with increasing the weight ratio of the copolymer poly (3HT - Co - Th).



Figure 2: UV- Visible absorbance spectra of the poly (3HT - Co - Th) - PMMA polymer blend film at different weight ratios of the copolymer poly (3HT - Co - Th).

The normalized transmittance curves of the closed - aperture laser beam z - scan, the open - aperture laser beam z - scan, and the pure nonlinear refraction of the p (3HT - Co - Th) - PMMA polymer blend film at different weight ratios of the copolymer poly (3HT - Co - Th) were measured and are shown in Figs.3 (a) - (c), respectively. The contribution of the nonlinear refraction only (the pure normalized transmittance curves in Fig. 3 (c)) was obtained by dividing the data of the normalized transmittance of the closed - aperture laser beam z - scan by the data of the normalized transmittance of the closed - aperture laser beam z - scan by the data of the normalized transmittance of the closed - aperture laser beam z - scan by the data of the normalized transmittance of the closed - aperture laser beam z - scan by the data of the normalized transmittance of the closed - aperture laser beam z - scan by the data of the normalized transmittance of the closed - aperture laser beam z - scan by the data of the normalized transmittance of the closed - aperture laser beam z - scan by the data of the normalized transmittance of the closed - aperture laser beam z - scan by the data of the normalized transmittance of the closed - aperture laser beam z - scan by the data of the normalized transmittance curve starts with a peak in the negative part of the z - axis to the valley in the positive part of the z - axis, this means that the normalized transmittance curve has a peak - to - valley feature. Such behavior is an indication of the exhibiting of self - defocusing effect of the laser beam when passing through the polymer film

samples, and thus these film samples have negative values of the nonlinear refractive index ($n_2 < 0$). It is clear from Fig. 3 (b) that there is an increase in the value of the normalized transmittance when the sample approaches the focal point, and this gives an indication that the prepared film samples in the present study exhibit saturable absorption (SA) when the laser beam intensity increases, and this means that these film samples have negative values of the nonlinear absorption coefficient ($\beta < 0$).



Figure 3: Normalized transmittance curves for the poly (3HT - Co - Th) - PMMA polymer blend film at different weight ratios of the copolymer poly (3HT - Co - Th). (a) Closed - aperture z - scan. (b) Open - aperture z - scan. (c) Pure nonlinear refraction.

The nonlinear optical parameters, n_2 , β , and the real (Re (χ ⁽³⁾)) and the imaginary (Im (χ ⁽³⁾)) parts of the third - order nonlinear optical susceptibility ((χ ⁽³⁾)) can be determined from the following relations.

By Using the difference between peak and valley transmittances for the normalized transmission curve i.e., $\Delta T_{p-y} = T_p - T_y$, the phase difference $\Delta \phi_0$ can be determined according to the following relation [25, 26]:

$$\Delta T_{p-v} = 0.406 (1 - S)^{0.25} |\Delta \phi_0|$$
⁽¹⁾

where S is the linear transmittance of the aperture and given by:

$$S = 1 - \exp(-2 r_a^2 / w_a^2)$$
(2)

where rais the radius of the aperture and wa is the radius of the laser beam at the entrance of the aperture and given by:

$$w_{a} = w_{o} \left[1 + \left(\frac{\lambda z_{a}}{\pi w_{o}^{2}} \right)^{2} \right]^{\frac{1}{2}}$$
(3)

where λ is the wavelength of the laser beam.

Figure 4: shows the calculated peak - valley transmittance difference (ΔT_{p-v}) as a function of the copolymer poly (3HT - Co - Th) weight ratio. It is seen that the value of ΔT_{P-v} increases with increasing the weight ratio of the copolymer poly (3HT - Co - Th).

sociated with the real (Re (χ ⁽³⁾)) and the imaginary (Im (χ ⁽³⁾)) The non parts of the third - order nonlinear optical susceptibility (χ ⁽³⁾), and provide important information about the properties of the material. The real and the imaginary parts of the third - order nonlinear optical susceptibility can be determined by using the following relations [30]:

Figure 4: Variation of ΔT_{p-v} with the weight ratio of the copolymer poly (3HT - Co - Th).

The nonlinear refractive index (n_2) is given by the following relation [26]:

$$\mathbf{n}_2 = \frac{\Delta \Theta_0 \ \lambda}{2 \ \pi \ \mathbf{I}_0 \ \mathbf{L}_{\text{effl}}} \tag{4}$$

where I_0 is the intensity of the laser beam at focus (z = 0), and given by:

$$\mathbf{I}_0 = \frac{2 \mathbf{P}_0}{\pi \omega_0^2} \tag{5}$$

where
$$P_0$$
 is the laser input power.

The induced refractive index change (Δ n) of material is given by the relation:

$$\Delta \mathbf{n} = \mathbf{n}_2 \mathbf{I} \tag{6}$$

where I is the intensity of the incident laser beam.

The nonlinear absorption coefficient (β) is given by the following relation:

$$\beta = \frac{2\sqrt{2}}{I_0 L_{eff}} \Delta T$$

where ΔT is the normalized transmittance difference between peak at the focal point (z = 0) in the open aperture z - scan normalized transmittance curve and the baseline, and L_{eff} is the effective length of the sample and given by:

$$\mathbf{L}_{\mathrm{eff}} = \left(1 - \exp\left(-\alpha_0 \mathbf{L}\right)\right) / \alpha_0$$

linear optical parameters
$$n_2$$
 and β are associated with the real (Re (χ ⁽³⁾)) and

(8)



Re
$$[\chi^{(3)}]$$
 (esu) = 10⁻⁴ $\frac{\varepsilon_0 c^2 n_0^2 n_2}{\pi}$ (cm²/W) (9)

Im
$$[\chi^{(3)}]$$
 (esu) = $10^{-2} - \frac{\epsilon_0 c^2 n_0^2 \lambda \beta}{4 \pi^2}$ (cm / W) (10)

The complex third - order nonlinear optical susceptibility ($\chi^{(3)}$), can be described by the following relation:

$$|\chi^{(3)}| = \left[\left(\operatorname{Re} \left(\chi^{(3)} \right) \right)^2 + \left(\operatorname{Im} \left(\chi^{(3)} \right) \right)^2 \right]^{\frac{1}{2}}$$
(11)

The nonlinear refractive index (n_2), the nonlinear absorption coefficient (β), and the third - order nonlinear optical susceptibility ($|\chi^{(3)}|$) were plotted as a function of the weight ratio of the copolymer poly (3HT - Co - Th), as shown in Figs. 5, 6 and 7, respectively. The calculated values of the optical parameters of the prepared poly (3HT - Co - Th) - PMMA polymer blend film for different weight ratios of the copolymer poly (3HT - Co - Th), are summarized in Table 1. It is clearly noticed from this table; the values of the nonlinear optical parameters increase with increasing the weight ratio of the copolymer poly (3HT - Co - Th).



Figure 5: The nonlinear refractive index (n₂) of the poly (3HT - Co - Th) - PMMA polymer blend film as a function of the weight ratio of the copolymer poly (3HT - Co - Th).



Figure 6: The nonlinear absorption coefficient (β) of the poly (3HT - Co - Th) - PMMA polymer blend film as a function of the weight ratio of the copolymer poly (3HT - Co - Th).



Figure 7: The nonlinear third - order optical susceptibility ($|\chi^{(3)}|$) of the poly (3HT - Co - Th) - PMMA polymer blend film as a function of the weight ratio of the copolymer poly (3HT - Co - Th).

Table 1: The calculated values of the optical parameters of poly (3HT - Co - Th) - PMMA polymer blend film for five different weight ratios of the copolymer poly (3HT - Co - Th).

	1	A 75		· · · · · ·				
poly (3HT-Co-Th)	no	ΔT_{p-v}	n_2	Δn	β	RelX ⁽³⁾	$Im[\chi^{(3)}]$	$\chi^{(3)}$
(%)			(cm^2/W)		(cm/W)	(esu)	(esu)	(esu)
			×10 ⁻⁸	×10-4	×10-3	×10 ⁻⁶	×10 ⁻⁶	×10 ⁻⁶
0.033	1.42	0.45	0.07	0.13	0.01	0.89	0.82	1.21
0.040	1.53	0.55	0.13	0.25	0.03	1.69	1.82	2.48
0.046	1.90	0.68	0.48	0.95	0.12	7.22	7.65	10.5
0.053	2.15	0.86	1.08	2.13	0.27	17.4	17.8	24.9
0.060	2.43	1.03	1.75	3.45	0.41	30.3	29.4	42.2

The optical power limiting properties of the poly (3HT - Co - Th) - PMMA polymer blend film for different weight ratios of the copolymer poly (3HT - Co - Th) were also studied. Optical power limiting effect was study by using the z - scan technique. The sample of the poly (3HT - Co - Th) - PMMA polymer blend film was fixed in the z - scan system after the focal point of the lens, and the laser input power was varied progressively and the corresponding laser output power was recorded by the photo-detector D₂. Fig. 8 shows the optical power limiting curves (the laser output power versus the laser input power) for the poly (3HT - Co - Th) - PMMA polymer blend film at different weight ratios of the copolymer poly (3HT - Co - Th). From this figure, it is noticed that the laser input power - laser output power characteristic shape depends on the weight ratio of the copolymer poly (3HT - Co - Th). The poly (3HT - Co - Th) - PMMA polymer blend film starts to show more obvious power limiting behavior with increasing the weight ratio of the copolymer poly (3HT - Co - Th). Because an increase in the weight ratio of the copolymer poly (3HT - Co - Th). Because an increase in the weight ratio of the copolymer poly (3HT - Co - Th). Because an increase in the weight ratio of the copolymer poly (3HT - Co - Th). Because an increase in the weight ratio of the copolymer poly (3HT - Co - Th). Because an increase in the weight ratio of the copolymer poly (3HT - Co - Th).

The values of the optical power threshold (P_{th}) of the optical power limiter of the prepared poly (3HT - Co - Th) - PMMA polymer blend film was determined for the different weight ratios of the copolymer poly (3HT - Co - Th). The estimated values of the optical power threshold (P_{th}) of the poly (3HT - Co - Th) - PMMA polymer blend film for different weight ratios of the copolymer poly (3HT - Co - Th) are shown in Table 2. It can be noticed that the value of the optical power threshold (P_{th}) depends on the weight ratio of the copolymer poly (3HT - Co - Th), and it decreases with increasing the weight ratio of the copolymer poly (3HT - Co - Th).



Figure 8: Optical power limiting of the poly (3HT - Co - Th) - PMMA polymer blend film for different weight ratios of the copolymer poly (3HT - Co - Th).

Table 2: The estimated values of the optical power threshold (Pth) of the poly (3HT - Co - Th) - PMMA polymerblend film for different weight ratios of the copolymer poly (3HT - Co - Th).

Poly (3HT - Co -Th)	Optical power threshold (P _{th})				
(%)	(mW)				
0.033	24				
0.040	18				
0.046	13				
0.053	11				
0.060	8				

4. CONCLUSIONS

The copolymer poly (3HT - Co - Th) was prepared by using the addition polymerization method and the film samples of the poly (3HT - Co - Th) - PMMA polymer blend were prepared, for different weight ratios of the copolymer poly (3HT - Co - Th), by using the casting method. The nonlinear optical properties and the behavior of the optical power limiting of the prepared poly (3HT - Co - Th) - PMMA blend polymer film sample for different weight ratios of the copolymer poly (3HT - Co - Th) were studied. The nonlinear optical parameters of the prepared poly (3HT - Co - Th) - PMMA polymer blend film samples, the refractive index (n₂), the nonlinear absorption coefficient (β), and the third - order optical susceptibility ($|\chi^{(3)}|$) were measured by using the z - scan technique with a continuous wave (CW) diode - pumped solid - state laser (DPSSL) operating at the wavelength 532 nm. It is observed that the prepared poly (3HT - Co - Th) - PMMA polymer blend sample films exhibit the effects of the self - defocusing and the nonlinear saturable absorption (SA), which is the indication of the negative values for both the nonlinear refractive index and the nonlinear absorption coefficient (n₂ < 0 and β < 0). Obtained results show that increasing of the weight ratio of the copolymer poly (3HT - Co - Th) in the poly (3HT - Co - Th) - PMMA polymer blend film sample. Also, increasing of the weight ratio of the copolymer poly (3HT - Co - Th) in the poly (3HT - Co - Th) - PMMA polymer blend film sample will increase the values of the nonlinear optical parameters, n₂, β , and $|\chi^{(3)}|$), of this polymer blend film sample.

The optical power limiting behavior of the poly (3HT - Co - Th) - PMMA blend polymer film was studied for different weight ratios of the copolymer poly (3HT - Co - Th). The obtained results showed that the prepared blend polymer films exhibit clear optical power limiting with reasonably low power limiting threshold (P_{th}). Results indicate that the prepared poly (3HT - Co - Th) - PMMA polymer blend films are promising candidates, can be used as potential materials for different optical and electronic applications, such as, optical power limiters, optical sensors, solar cells, and other optical and optoelectronic devices.

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CONFLICT OF INTEREST

The author have declared that no competing interests exist.

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